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Attached hereto is a marked-up version of the changes made to the specification by the current amendment. The attached page is captioned "Version With Markings To Show Changes Made."

Respectfully submitted,

CHABOT

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Version With Markings To Show Changes Made

IN THE SPECIFICATION:

The following paragraph has been inserted at page 1, before line 1:

This application claims priority under 35 USC § 119(e)(1) of provisional application number 60/236,532 filed 09/29/00.

Page 1, lines 5-9: have been deleted in its entirety and replaced as follows:

Patent No.	Filing Date	Issue Date	Title
5,061,049	Sept. 13, 1990	Oct. 29, 1991	Spatial Light Modulator and Method
5,583,688	Dec. 21, 1993	Dec. 10, 1996	Multi-Level Digital Micromirror Device
60/223,366	Aug. 7, 2000		Two Dimensional Blazed Grating
TI-29776	Herewith		Micromirror Optical Switch
TI-29778	Herewith		Micromirror Optical Switch

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<u>5,061,049</u>	<u>Sept. 13, 1990</u>	<u>Oct. 29, 1991</u>	<u>Spatial Light Modulator and Method</u>
<u>5,583,688</u>	<u>Dec. 21, 1993</u>	<u>Dec. 10, 1996</u>	<u>Multi-Level Digital Micromirror Device</u>
<u>09/923,911</u>	<u>Aug. 7, 2001</u>		<u>Two Dimensional Blazed MEMS Grating</u>
<u>60/236,533</u>	<u>Sept. 29, 2000</u>		<u>Micromirror Optical Switch</u>
<u>60/236,677</u>	<u>Sept. 29, 2000</u>		<u>Micromirror Optical Switch</u>

The paragraph beginning on line 21 of page 17 has been amended as follows:

When small mirrors, mirrors smaller than the beam cross-section, are used, the mirror rotations angles should be selected to ensure blazed operation of the mirror array. Mirrors in common micromirror devices are 16 μm on each side and spaced 1 μm from the surrounding mirrors. As described in U.S. Patent Application Serial No. ~~60/223,366~~ 09/923,911, proper selection of the deflection angle ensures the array operates in an efficient blazed condition. For mirrors on 17 μm centers, as described above, ideal deflection angles are ~~9.6° and 13.8°~~, 7.5° and 11.2°, which blaze the 2nd and 3rd orders respectively. For mirrors on 13.8 μm centers, a deflection angle of 9.6° blazes the 2nd order.

The paragraph beginning on line 10 of page 20 has been amended as follows:

Figure 12 is a side view of another beam splitting device used in the DWDM OADM of Figure 9. In Figure 12, light from the input fiber 1000 enters an arrayed waveguide grating, ~~also known as a PHASAR~~. The arrayed waveguide grating router includes a series of arrayed channel waveguides which function as a diffraction grating. The arrayed waveguide grating enables the use of more than forty DWDM channels.

Light separated by the arrayed waveguide grating is output on a series of fibers 1202 to the mirror array 1008 of the OADM.

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